

### Chapter 7: Deformation & Strengthening Mechanisms

**ISSUES TO ADDRESS...**

- Why are the number of \_\_\_\_\_ present greatest in metals?
- How are strength and \_\_\_\_\_ related?
- Why does heating alter strength and other properties?

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### Dislocations & Materials Classes

- \_\_\_\_\_ (Cu, Al):  
Dislocation motion easiest  
- non-directional bonding  
- close-packed directions for slip
- \_\_\_\_\_ (Si, diamond): Motion difficult  
- directional (angular) bonding
- \_\_\_\_\_ (NaCl):  
Motion difficult  
- need to avoid nearest \_\_\_\_\_ of like sign (- and +)

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### Dislocation Motion

Dislocation motion & plastic \_\_\_\_\_

- Metals - plastic \_\_\_\_\_ occurs by **slip** – an edge dislocation (extra half-plane of atoms) slides over adjacent plane half-planes of atoms.

(a)

(b)

(c)

Adapted from Fig. 7.1, Callister & Rethwisch 8e

- If dislocations can't move, plastic \_\_\_\_\_ doesn't occur!

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### Dislocation Motion

- A dislocation moves along a slip plane in a slip direction perpendicular to the dislocation line
- The slip direction is the same as the direction

Adapted from Fig. 7.2, Callister & Rethwisch 8e.

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### Deformation Mechanisms

#### Slip System

- plane on which easiest occurs
  - Highest planar (and large interplanar spacings)
- Slip directions of movement
  - Highest densities

Adapted from Fig. 7.6, Callister & Rethwisch 8e.

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### Stress and Dislocation Motion

- Resolved results from applied

Applied stress:  $\sigma = F/A$       Resolved stress:  $\tau_R = F_S/A_S$       Relation between  $\sigma$  and  $\tau_R$

$\tau_R = \sigma \cos \lambda \cos \phi$

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### Critical Resolved Shear Stress

- Condition for plastic motion:  $\tau_R > \tau_{CRSS}$
- Ease of plastic motion depends on crystal orientation typically  $10^{-4}$  GPa to  $10^{-2}$  GPa

$$\tau_R = \sigma \cos \lambda \cos \phi$$

$\tau$  maximum at  $\lambda = \phi = 45^\circ$

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### Single Crystal Slip

Adapted from Fig. 7.8, Callister & Rethwisch 8e.

Adapted from Fig. 7.9, Callister & Rethwisch 8e.

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### Ex: Deformation of single crystal

a) Will the single crystal yield?  
b) If not, what stress is needed?

$\phi = 60^\circ$   
 $\lambda = 35^\circ$

$\tau_{CRSS} = \underline{\hspace{2cm}}$

$$\tau = \sigma \cos \lambda \cos \phi$$

$$\sigma = 45 \text{ MPa}$$

$$\tau = (45 \text{ MPa}) (\cos 35^\circ) (\cos 60^\circ)$$

$$= (45 \text{ MPa}) (0.41)$$

$$\tau = 18.4 \text{ MPa} < \tau_{CRSS} = \underline{\hspace{2cm}}$$

$\sigma = \underline{\hspace{2cm}}$

So the applied stress will not cause the crystal to yield.

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### Ex: Deformation of single crystal

What stress is necessary (i.e., what is the \_\_\_\_\_,  $\sigma_y$ )?

$$\tau_{crss} = 20.7 \text{ MPa} = \sigma_y \cos \lambda \cos \phi = \sigma_y (0.41)$$

$$\therefore \sigma_y = \frac{\tau_{crss}}{\cos \lambda \cos \phi} = \frac{20.7 \text{ MPa}}{0.41} = 50.5 \text{ MPa}$$

So for deformation to occur the \_\_\_\_\_ must be greater than or equal to the \_\_\_\_\_

$$\sigma \geq \sigma_y = 50.5 \text{ MPa}$$

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### Slip Motion in Polycrystals

- \_\_\_\_\_ stronger than single crystals – grain boundaries are barriers to dislocation motion.
- Slip planes & directions ( $\lambda$ ,  $\phi$ ) change from one grain to another.
- \_\_\_\_\_ from one grain to another.
- The grain with the largest  $\tau_R$  yields first.
- Other (less favorably oriented) grains yield later.



Adapted from Fig. 7.10, Callister & Rethwisch 8e (Fig. 7.10 is courtesy of C. Brady, National Bureau of Standards [now the National Institute of Standards and Technology, Gaithersburg, MD].)

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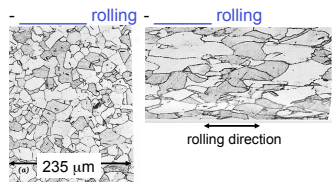
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### Anisotropy in $\sigma_y$

- Can be induced by rolling a \_\_\_\_\_ metal



Adapted from Fig. 7.11, Callister & Rethwisch 8e (Fig. 7.11 is from W.G. Moffatt, G.W. Pearsall, and J. Wulff, The Structure and Properties of Materials, Vol. I, Structure, p. 140, John Wiley and Sons, New York, 1964.)

since grains are equiaxed & \_\_\_\_\_ oriented.

since rolling affects grain \_\_\_\_\_ and shape.

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### Anisotropy in Deformation

1. Cylinder of machined from a rolled plate:

2. Fire cylinder at a target.

3. Deformed cylinder

Photos courtesy of G.T. Gray III, Los Alamos National Labs. Used with permission.

• The noncircular end view shows \_\_\_\_\_ deformation of rolled material.

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### Four Strategies for Strengthening: 1: Reduce Grain Size

- Grain boundaries are barriers to slip.
- Barrier "strength" \_\_\_\_\_ with increasing angle of misorientation.
- \_\_\_\_\_ grain size: more barriers to slip.

Adapted from Fig. 7.14, Callister & Rethwisch 8e. (Fig. 7.14 is from A Textbook of Materials Technology, by Van Vlack, Pearson Education, Inc., Upper Saddle River, NJ.)

• Hall-Petch Equation:  $\sigma_{yield} = \sigma_o + k_y d^{-1/2}$

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### Four Strategies for Strengthening: 2: Form Solid Solutions

- Impurity atoms distort the \_\_\_\_\_ & generate lattice strains.
- These strains can act as barriers to \_\_\_\_\_ motion.

• Smaller substitutional impurity

Impurity generates local stress at **A** and **B** that opposes dislocation motion to the right.

• Larger substitutional impurity

Impurity generates local stress at **C** and **D** that opposes dislocation motion to the right.

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### Lattice Strains Around Dislocations

Adapted from Fig. 7.4,  
Callister & Rethwisch 8e.

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### Strengthening by Solid Solution Alloying

- Small \_\_\_\_\_ tend to concentrate at dislocations (regions of \_\_\_\_\_ strains) - partial cancellation of dislocation compressive strains and impurity atom tensile strains
- Reduce mobility of \_\_\_\_\_ and increase strength

Adapted from Fig. 7.17,  
Callister & Rethwisch 8e.

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### Strengthening by Solid Solution Alloying

- Large \_\_\_\_\_ tend to concentrate at \_\_\_\_\_ (regions of tensile strains)

Adapted from Fig. 7.18,  
Callister & Rethwisch 8e.

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### VMSE Solid-Solution Strengthening Tutorial

**Solid-Solution Strengthening**

This module allows you to observe the mechanism of solid solution strengthening by viewing animations, which are accompanied with voice-overs.

Pure

Larger

Smaller

Interstitial

Help

Please be patient. This may take a few minutes to load depending on your connection speed.

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### Ex: Solid Solution Strengthening in Copper

- Tensile strength & yield strength increase with wt% Ni.

Adapted from Fig. 7.16(a) and (b), Callister & Rethwisch 8e.

- \_\_\_\_\_ relation:  $\sigma_y \sim C^{1/2}$
- \_\_\_\_\_ increases  $S_y$  and  $TS$ .

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### Four Strategies for Strengthening: 3: \_\_\_\_\_ Strengthening

- Hard \_\_\_\_\_ are difficult to shear.  
Ex: \_\_\_\_\_ in metals (SiC in Iron or \_\_\_\_\_).

Side View

Top View

- Result:  $\sigma_y \sim \frac{1}{S}$

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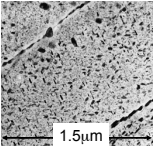
### Application: Precipitation \_\_\_\_\_

- Internal wing structure on Boeing 767



Adapted from chapter-opening photograph, Chapter 11, Callister & Rethwisch 8e. (courtesy of G.H. Narayanan and A.G. Miller, Boeing Commercial Airplane Company.)

- Aluminum is strengthened with \_\_\_\_\_ formed by alloying.



Adapted from Fig. 11.26, Callister & Rethwisch 8e. (Fig. 11.26 is courtesy of G.H. Narayanan and A.G. Miller, Boeing Commercial Airplane Company.)

1.5µm

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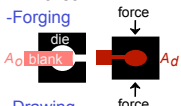
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### Four Strategies for Strengthening: 4: Cold Work (Strain \_\_\_\_\_)

- Deformation at room temperature (for most metals).
- Common \_\_\_\_\_ reduce the cross-sectional area:

**-Forging**



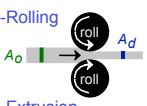
force

die

$A_0$  blank

$A_d$

**-Rolling**




roll

$A_0$

$A_d$

**-Drawing**




die

$A_0$

$A_d$

tensile force

**-Extrusion**



container

die holder

force

ram

billet

extrusion

die

$A_0$

$A_d$

$$\%CW = \frac{A_0 - A_d}{A_0} \times 100$$

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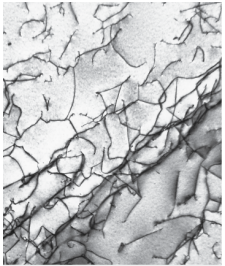
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### Dislocation Structures Change During Cold Working

- \_\_\_\_\_ structure in Ti after cold \_\_\_\_\_.



0.2 µm

- Dislocations entangle with one another during \_\_\_\_\_.
- \_\_\_\_\_ motion becomes more difficult.

Fig. 4.6, Callister & Rethwisch 8e. (Fig. 4.6 is courtesy of M.R. Plichta, Michigan Technological University.)

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### Dislocation Density Increases During Cold Working

Dislocation density =  $\frac{\text{total dislocation length}}{\text{unit volume}}$

- Carefully grown \_\_\_\_\_  
→ ca.  $10^3 \text{ mm}^{-2}$
- Deforming sample \_\_\_\_\_ density  
→  $10^9\text{-}10^{10} \text{ mm}^{-2}$
- Heat treatment \_\_\_\_\_ density  
→  $10^5\text{-}10^6 \text{ mm}^{-2}$

• Yield stress \_\_\_\_\_ as  $\rho_d$  increases:

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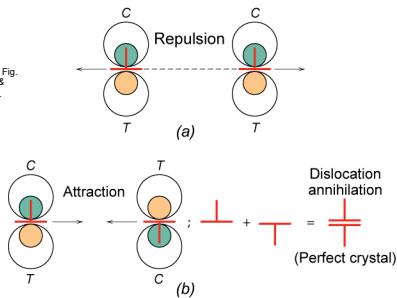
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### Lattice Strain Interactions Between Dislocations

Adapted from Fig. 7.5, Callister & Rethwisch 8e.



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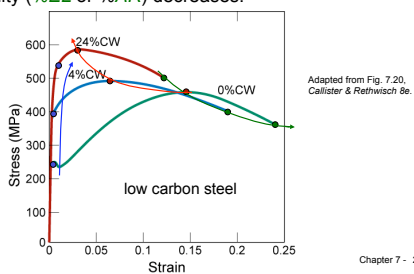
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### Impact of Cold Work

As cold work is increased

- \_\_\_\_\_ strength ( $\sigma_y$ ) increases.
- Tensile strength ( $TS$ ) \_\_\_\_\_.
- Ductility ( $\%EL$  or  $\%AR$ ) decreases.



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### Mechanical Property Alterations Due to

- What are the values of yield strength, tensile strength &                      after cold working Cu?

Copper  
Cold  
Work

$D_0 = 15.2 \text{ mm}$        $D_d = 12.2 \text{ mm}$

$$\%CW = \frac{\frac{\pi D_0^2}{4} - \frac{\pi D_d^2}{4}}{\frac{\pi D_0^2}{4}} \times 100$$

$$= \frac{D_0^2 - D_d^2}{D_0^2} \times 100$$

$$\%CW = \frac{(15.2 \text{ mm})^2 - (12.2 \text{ mm})^2}{(15.2 \text{ mm})^2} \times 100 = 35.6\%$$

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### Mechanical Property Alterations Due to Cold Working

- What are the values of yield strength,                      & ductility for Cu for %CW = 35.6%?

Yield strength (MPa)

300 MPa      340 MPa

0      20      40      60

% Cold Work

$\sigma_y =$

tensile strength (MPa)

340 MPa      380 MPa

0      20      40      60

% Cold Work

TS =

ductility (%EL)

7%      3%

0      20      40      60

% Cold Work

%EL =

Adapted from Fig. 7.19, Callister & Rethwisch 8e. (Fig. 7.19 is adapted from Metals Handbook: Properties and Selection: Iron and Steels, Vol. 1, 9th ed., B. Bardes (Ed.), American Society for Metals, 1978, p. 226; and Metals Handbook: Properties and Selection: Nonferrous Alloys and Pure Metals, Vol. 2, 9th ed., H. Baker (Managing Ed.), American Society for Metals, 1979, p. 276 and 327.)

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### Effect of Heat Treating After Cold Working

- 1 hour treatment at  $T_{anneal}$ ... decreases TS and increases %EL.
- Effects of cold work are nullified!

annealing temperature (°C)

tensile strength (MPa)

ductility (%EL)

Recovery      Recrystallization      Grain Growth

- Three Annealing stages:
  - 
  - 
  - Grain Growth

Adapted from Fig. 7.22, Callister & Rethwisch 8e. (Fig. 7.22 is adapted from G. Sachs and K.R. van Horn, Practical Metallurgy: Applied Metallurgy, and the Industrial Processing of Ferrous and Nonferrous Metals and Alloys, American Society for Metals, 1940, p. 139.)

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### Three Stages During Heat Treatment:

#### 1. Recovery

Reduction of \_\_\_\_\_ density by annihilation.

- Scenario 1 Results from \_\_\_\_\_
  - extra half-plane of atoms
  - atoms diffuse to regions of tension
  - extra half-plane of atoms
  - Dislocations annihilate and form a perfect atomic plane.
- Scenario 2
  - 3. "Climbed" disl. can now move on new slip plane
  - 2. grey atoms leave by vacancy diffusion allowing disl. to "climb"
  - 1. dislocation blocked; can't move to the right
  - 4. opposite dislocations meet and annihilate
  - Obstacle dislocation

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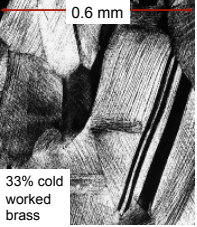
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### Three Stages During Heat Treatment:

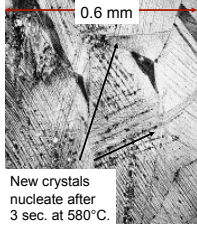
#### 2. \_\_\_\_\_

- New grains are formed that:
  - have low \_\_\_\_\_ densities
  - are small in \_\_\_\_\_
  - consume and replace parent cold-worked grains.



0.6 mm

33% cold worked brass



0.6 mm

New crystals nucleate after 3 sec. at 580°C.

Adapted from Fig. 7.21(a),(b), Callister & Rethwisch 8e. (Fig. 7.21(a),(b) are courtesy of J.E. Burke, General Electric Company.)

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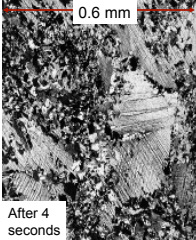
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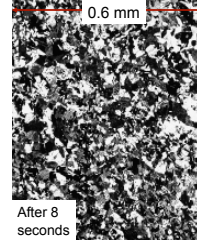
### As Recrystallization Continues...

- All \_\_\_\_\_ are eventually consumed/replaced.



0.6 mm

After 4 seconds



0.6 mm

After 8 seconds

Adapted from Fig. 7.21(c),(d), Callister & Rethwisch 8e. (Fig. 7.21(c),(d) are courtesy of J.E. Burke, General Electric Company.)

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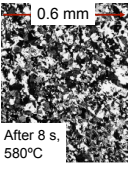
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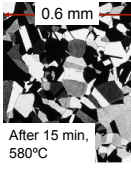
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### Three Stages During Heat Treatment: 3. Grain Growth

- At longer times, average grain size increases.
  - Small \_\_\_\_\_ (and ultimately disappear)
  - Large \_\_\_\_\_ continue to grow



After 8 s,  
580°C



After 15 min,  
580°C

Adapted from Fig. 7.21(d),(e), Callister & Rethwisch 8e. (Fig. 7.21(d),(e) are courtesy of J.E. Burke, General Electric Company.)

Empirical Relation:  
 $d^n - d_0^n = Kt$   
 exponent typ. ~ 2 on grain diam. at time t.      coefficient on elapsed time

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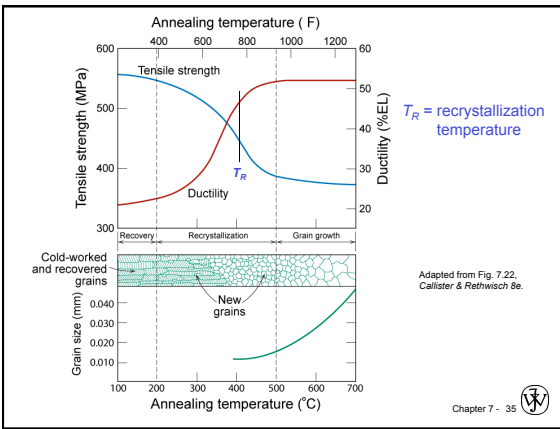
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### Recrystallization Temperature

T<sub>R</sub> = \_\_\_\_\_ temperature = temperature at which \_\_\_\_\_ completion in 1 h.

$$0.3T_m < T_R < 0.6T_m$$

For a specific metal/alloy, T<sub>R</sub> depends on:

- %CW -- T<sub>R</sub> decreases with increasing %CW
- Purity of \_\_\_\_\_ -- T<sub>R</sub> decreases with increasing purity

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### Diameter Reduction Procedure - Problem

A cylindrical rod of \_\_\_\_\_ in diameter is to be cold worked by drawing. The circular cross section will be maintained during deformation. A cold-worked tensile strength in excess of \_\_\_\_\_ and a ductility of at least 15 %EL are desired. Furthermore, the final diameter must be 7.5 mm (0.30 in). Explain how this may be accomplished.

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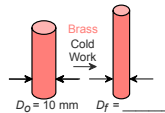
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### Diameter Reduction Procedure - Solution

What are the consequences of directly drawing to the final diameter?



$$\%CW = \left( \frac{A_o - A_f}{A_o} \right) \times 100 = \left( 1 - \frac{A_f}{A_o} \right) \times 100$$

$$= \left( 1 - \frac{\pi D_f^2 / 4}{\pi D_o^2 / 4} \right) \times 100 = \left( 1 - \left( \frac{7.5}{10} \right)^2 \right) \times 100 = 43.8\%$$

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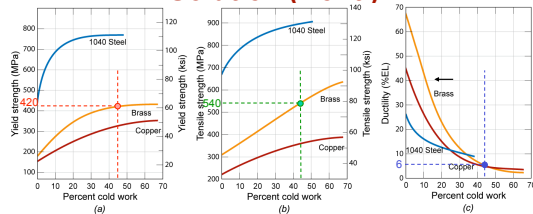
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### Diameter Reduction Procedure - Solution (Cont.)



- For %CW = 43.8%
  - $\sigma_y =$  \_\_\_\_\_
  - T<sub>S</sub> = \_\_\_\_\_ 380 MPa
  - %EL = \_\_\_\_\_ 15
- This doesn't satisfy criteria... what other options are possible?

Adapted from Fig. 7.19, Callister & Rethwisch 6e.

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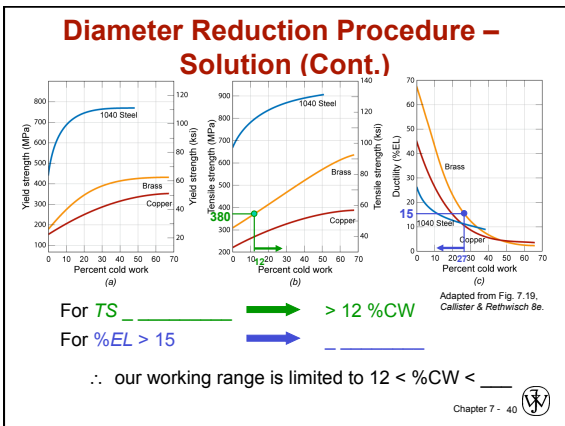
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### Diameter Reduction Procedure – Solution (cont.)

Cold work, then \_\_\_\_\_, then \_\_\_\_\_ again

- For objective we need a cold work of  $12 < \%CW < 27$ 
  - We'll use 20 %CW
- Diameter after first cold work stage (but before 2<sup>nd</sup> cold work stage) is calculated as follows:

$$\%CW = \left(1 - \frac{D_{f2}^2}{D_{02}^2}\right) \times 100 \Rightarrow 1 - \frac{D_{f2}^2}{D_{02}^2} = \frac{\%CW}{100}$$

$$\frac{D_{f2}}{D_{02}} = \left(1 - \frac{\%CW}{100}\right)^{0.5} \Rightarrow D_{02} = \frac{D_{f2}}{\left(1 - \frac{\%CW}{100}\right)^{0.5}}$$

Intermediate diameter =  $D_{f1} = D_{02} = 7.5 \text{ mm} / \left(1 - \frac{20}{100}\right)^{0.5} = 8.39 \text{ mm}$

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### Diameter Reduction Procedure – Summary

Stage 1: \_\_\_\_\_ – reduce diameter from 10 mm to 8.39 mm

$$\%CW_1 = \left(1 - \left(\frac{8.39 \text{ mm}}{10 \text{ mm}}\right)^2\right) \times 100 = 29.6$$

Stage 2: \_\_\_\_\_ (allow recrystallization)

Stage 3: \_\_\_\_\_ – reduce diameter from 8.39 mm to 7.5 mm

$$\%CW_2 = \left(1 - \left(\frac{7.5}{8.39}\right)^2\right) \times 100 = 20 \quad \Rightarrow \quad \text{Fig 7.19}$$

Therefore, all criteria satisfied

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### Cold Working vs. Hot Working

- Hot working → deformation above  $T_R$
- Cold working → deformation below  $T_R$

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### Grain Size Influences Properties

- Metals having \_\_\_\_\_ grains – relatively strong and tough at low temperatures
- Metals having \_\_\_\_\_ grains – good creep resistance at relatively \_\_\_\_\_ temperatures

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### Summary

- Dislocations are observed primarily in metals and alloys.
- Strength is increased by making dislocation motion difficult.
- Strength of metals may be increased by:
  - decreasing grain size
  - solid solution strengthening
  - precipitate hardening
  - cold working
- A cold-worked metal that is heat treated may experience recovery, recrystallization, and grain growth – its properties will be altered.

Chapter 7 - 45 

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